Magnetically Coupled Circuits

- The circuits we have considered so far may be regarded as **conductively coupled**, because one loop affects the neighboring loop through current conduction.
- When two loops with or without contacts between them affect each other through the magnetic field generated by one of them, they are said to be **magnetically coupled**.
Mutual Inductance is the basic operating principal of many application such as transformer, magnetic levitation trains and other electrical component that interacts with another magnetic field.

These devices use magnetically coupled coils to transfer energy from one circuit to another.

But mutual inductance can also be a bad thing as “stray” or “leakage” inductance from a coil can interfere with the operation of another adjacent component by means of electromagnetic induction, so some form of protection may be needed.
The voltage is induced in a circuit whenever the flux linking (i.e., passing through) the circuit is changing and that the magnitude of the voltage is proportional to the rate of change of the flux linkages.

\[ e = N \frac{d\phi}{dt} \]

The polarity of the induced voltage is such as to oppose the cause producing it.
Because the induced voltage in tries to counter (i.e., opposes) changes in current, it is called Back or Counter EMF.

- It opposes only changes in current NOT prevent the current from changing; it only prevents it from changing abruptly.

- This Equation is sometimes shown with a minus sign.
- However, the minus sign is unnecessary. In circuit theory, we use the equation to determine the magnitude of the induced voltage and Lenz’s law to determine its polarity.

Since induced voltage is proportional to the rate of change of flux, and since flux is proportional to current, induced voltage will be proportional to the rate of change of current.

$$e = N \frac{d\phi}{dt}$$

$$e = L \frac{di}{dt}$$

L: self inductance in Henry.
Self Inductance

From both equations, we get:

\[ L \frac{di}{dt} = N \frac{d\phi}{dt} \]

\[ L = N \frac{d\phi}{di} \]

For Sinusoidal: \( \frac{d}{dt} = jw \)

\[ V = L (jw) i = j i X_L \]

For Linear System (coils with air-core not iron-core):

\[ L = N \frac{\phi}{i} \]

- Self-Inductance parameters

\[ L = \frac{N^2 \mu A}{l} \] (henries, H)

- \( \mu_0 \) is the permeability of free space (4.\( \pi \).10\(^{-7} \))
- \( \mu_r \) is the relative permeability of the soft iron core
- \( N \) is in the number of coil turns
- \( A \) is in the cross-sectional area in m\(^2\)
- \( l \) is the coils length in meters
When two inductors (or coils) are in a close proximity to each other, the magnetic flux caused by current in one coil links with the other coil, thereby inducing voltage in the latter.

- For the sake of simplicity, assume that the second inductor carries no current.
- The magnetic flux emanating from coil 1 has two components: One component links only coil 1, and another component links both coils.

\[ \phi_1 = \phi_{11} + \phi_{12} \]

Leakage Flux + Linkage Flux

1. The induced voltage in the first coil

\[ v_1 = N_1 \frac{d\phi_1}{di_1} \frac{di_1}{dt} = L_1 \frac{di_1}{dt} \]

\[ v_1 = N_1 \frac{d\phi_1}{dt} \]
2. The induced voltage in the 2\textsuperscript{nd} coil

\[ v_2 = N_2 \frac{d\phi_{12}}{dt} \]

\[ v_2 = N_2 \frac{d\phi_{12}}{dt} \frac{di_1}{dt} = M_{21} \frac{di_1}{dt} \]

where \( M_{21} \) is known as the mutual inductance of coil 2 with respect to coil 1.

\( M_{21} \) relates the induced voltage in coil 2 to the current in coil 1.

\( M_{21} \) relates the induced voltage in coil 2 to the current in coil 1.

Thus, the open-circuit mutual voltage (or induced voltage) across coil 2 is \( v_2 \)

Similarly:

\[ \phi_2 = \phi_{21} + \phi_{22} \]

\[ M_{12} = N_1 \frac{d\phi_{21}}{di_2} \]

\[ v_1 = M_{12} \frac{di_2}{dt} \]

Mutual Inductance is bilateral:

\[ M_{12} = M_{21} = M \]
Coupling Coefficient

Is the fraction of the total flux that links to both coils

\[ k \equiv \frac{\phi_{12}}{\phi_1} = \frac{\phi_{21}}{\phi_2} \]

\[
M^2 = \left( N_2 \frac{d\phi_{12}}{di_1} \right) \left( N_1 \frac{d\phi_{21}}{di_2} \right) = \left( N_2 \frac{d(k\phi_1)}{di_1} \right) \left( N_1 \frac{d(k\phi_2)}{di_2} \right) = k^2 \left( N_1 \frac{d\phi_1}{di_1} \right) \left( N_2 \frac{d\phi_2}{di_2} \right) = k^2 L_1 L_2
\]

\[
M = k\sqrt{L_1 L_2} \quad \text{or} \quad X_M = k\sqrt{X_1 X_2}
\]

If all of the flux links the coils without any leakage flux, then \( k = 1 \).

- The term **close coupling** is used when most of the flux links the coils, either by way of a magnetic core to contain the flux or by interleaving the turns of the coils directly over one another.

- The term **loose coupling** is used when Coils placed side-by-side without a core and have correspondingly low values of \( k \).
Analysis of Coupled Circuits

- The two coils are on a common core which channels the magnetic flux

- To determine the proper signs on the voltages of mutual inductance, apply the right-hand rule to each coil:

  If the fingers wrap around in the direction of the assumed current, the thumb points in the direction of the flux.

1. If fluxes $\phi_1$ and $\phi_2$ aid one another, then the signs on the voltages of mutual inductance are the same as the signs on the voltages of self-inductance
2. If they oppose each other; a minus sign is used

\[ R_1 i_1 + L_1 \frac{di_1}{dt} + M \frac{di_2}{dt} = v_1 \]
\[ R_2 i_2 + L_2 \frac{di_2}{dt} = M \frac{di_1}{dt} = v_2 \]
Polarities in Close Coupling

So in our case:

\[ R_1i_1 + L_1 \frac{di_1}{dt} - M \frac{di_2}{dt} = v_1 \]

\[ R_2i_2 + L_2 \frac{di_2}{dt} - M \frac{di_1}{dt} = v_2 \]

Assuming sinusoidal voltage sources,

\[ \frac{(R_1 + j\omega L_1)I_1 - j\omega MI_2}{-j\omega MI_1 + (R_2 + j\omega L_2)I_2} = V_1 \]

\[ \begin{bmatrix} R_1 + j\omega L_1 & -j\omega M \\ -j\omega M & R_2 + j\omega L_2 \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} V_1 \\ V_2 \end{bmatrix} \]
Passive loops Consideration:

- Source $V_1$ drives a current $i_1$, with a corresponding flux $\phi_1$ as shown.
- Now Lenz’s law implies that the polarity of the induced voltage in the second circuit will make a current through the second coil in such a direction as to create a flux opposing the main flux established by $i_1$ .

- When the switch is closed, flux $\phi_2$ will have the direction shown.
- The right-hand rule, with the thumb pointing in the direction of $\phi_2$, provides the direction of the natural current $i_2$.

The induced voltage is the driving voltage for the second circuit, as suggested in figure 14-6:

\[ R_1 i_1 + L_1 \frac{di_1}{dt} - M \frac{di_2}{dt} = v_1 \]
\[ R_2 i_2 + L_2 \frac{di_2}{dt} - M \frac{di_1}{dt} = 0 \]
1. **Series Aiding Coils**

\[ V = j\omega L_1 I + j\omega M I + j\omega L_2 I + j\omega M I \]
\[ = j\omega L_{eq} I \]
where \( L_{eq} = L_1 + L_2 + 2M \).

2. **Series opposing Coils**

\[ V = j\omega L_1 I - j\omega M I + j\omega L_2 I - j\omega M I \]
\[ = j\omega L_{eq} I \]
where \( L_{eq} = L_1 + L_2 - 2M \).

**Subtract both equations:**

\[ M = \frac{1}{4}(L_A - L_B) \]
1. Parallel Aiding Coils

\[ V = j \omega L_1 I_1 + j \omega M I_2 \]
\[ V = j \omega M I_1 + j \omega L_2 I_2 \]

Solving these equations for \( I_1 \) and \( I_2 \) yields:

\[ I_1 = \frac{V(L_2 - M)}{j \omega(L_1 L_2 - M^2)} \]
\[ I_2 = \frac{V(L_1 - M)}{j \omega(L_1 L_2 - M^2)} \]

Using KCL gives us:

\[ I = I_1 + I_2 = \frac{V(L_1 + L_2 - 2M)}{j \omega(L_1 L_2 - M^2)} = \frac{V}{j \omega L_{eq}} \]

\[ L_{eq} = \frac{L_1 L_2 - M^2}{L_1 + L_2 - 2M} \]

2. Parallel opposing Coils

\[ L_{eq} = \frac{L_1 L_2 - M^2}{L_1 + L_2 + 2M} \]
Since it is inconvenient to show the construction details of coils on a circuit schematic, we apply the dot convention in circuit analysis.

A dot is placed in the circuit at one end of each of the two magnetically coupled coils.

Steps to assign the dots:

a. Select a current direction in one coil and place a dot at the terminal where this current enters the winding.

b. Determine the corresponding flux by application of the right-hand rule.

c. The flux of the other winding, according to Lenz’s law, opposes the first flux.

d. Use the right-hand rule to find the natural current direction corresponding to this second flux.

e. Now place a dot at the terminal of the second winding where the natural current leaves the winding.
1. When the assumed currents both enter or both leave a pair of coupled coils by the dotted terminals, the signs on the M-terms will be the same as the signs on the L-terms.

2. If one current enters by a dotted terminal while the other leaves by a dotted terminal, the signs on the M-terms will be opposite to the signs on the L-terms.