



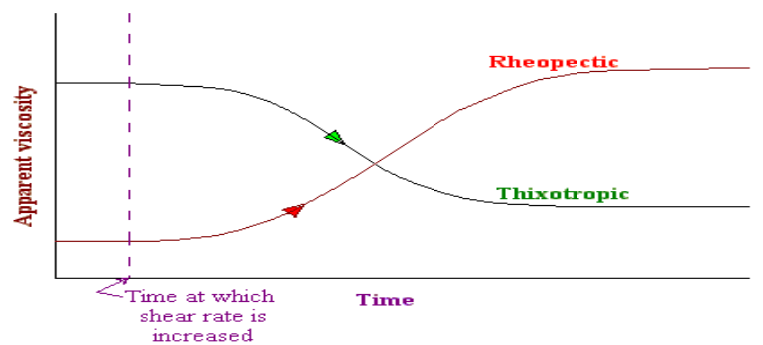
Benha University
Benha Higher Institute of Technology
Department of Mechanical Eng.

Subject: Fluid Mechanics Model Answer مادة ميكانيكا الموائع كود م ٢٠١
of the Final Exam Date: Jan./23/2011

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1-a) i) **Thixotropic fluids**: for which the dynamic viscosity decreases with the time for which shearing forces are applied. e.g. thixotropic jelly paints.

Rheopectic fluids: Dynamic viscosity increases with the time for which shearing forces are applied. e.g. gypsum suspension in water.



Effect of sudden change of shear rate on apparent viscosity of time-dependent fluids

ii) **Surface tension** is a phenomena that makes the interface between two fluids or between liquid and water behaves as elastic membrane.

iii) **Streakline** is a line passing through fluid particles originated from a given point (have earlier passed through a certain point in the flow field, **Timelines** are lines connecting specified particles at different time instants.

iv) **Visco-elastic fluids**: Some fluids have elastic properties, which allow them to spring back when a shear force is released. e.g. egg white.

v) **Potential flow**: Flow whose vorticity equal zero or $\text{Curl } \mathbf{V} = 0$

vi) **Fully developed fluid**: at certain distance from the entrance of the pipe, when the boundary layer reaches the center of the pipe the flow is called fully developed.

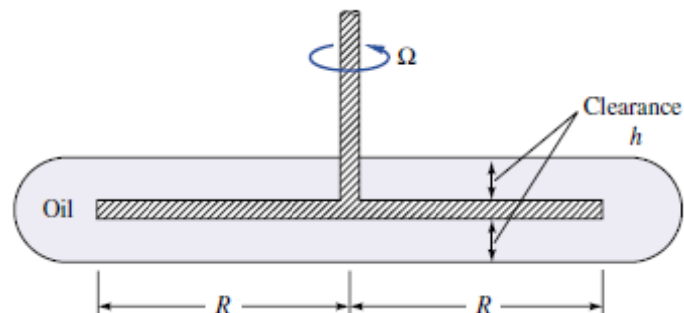
vii) **Boundary layer** : narrow region adjacent to the surface where the effect of the solid surface appears.

viii) **Entry length**: distance from the entrance of the pipe to the first section at which the flow becomes fully developed.

b) We find first the viscous torque (T) required:

$$dT = \tau dA \cdot r = \mu \frac{du}{dy} 2\pi r dr \cdot r = 2\pi\mu \frac{\Omega r}{h} r^2 dr$$

$$T = \frac{2\pi\mu\Omega}{h} \int_0^R r^3 dr = \frac{\pi\mu\Omega R^4}{2h}$$



$$T = 0.1822 N.m$$

$$power = T \cdot \Omega = 1.4577 \text{ watt}$$

c) Capillary rise or depression is given by the equation $h = \frac{4 \sigma \cos(\theta)}{\rho g d}$

$$h = -3.935 \text{ mm} \quad \text{depression}$$

2-a)

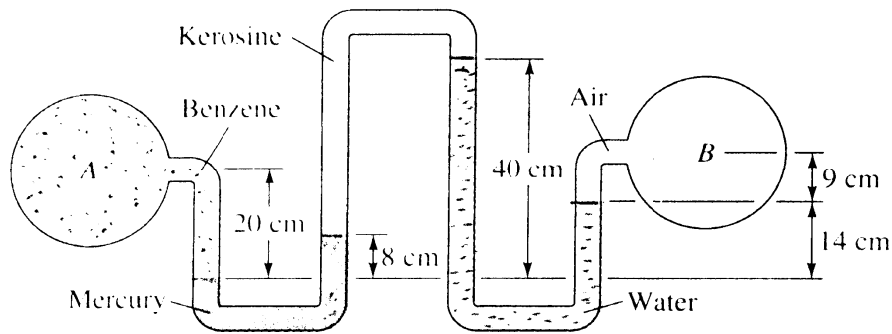


Figure 2

From figure 2 above we have:

$$P_A = 14.5 \text{ psi} = 1 \text{ bar} = 10^5 \text{ Pa}$$

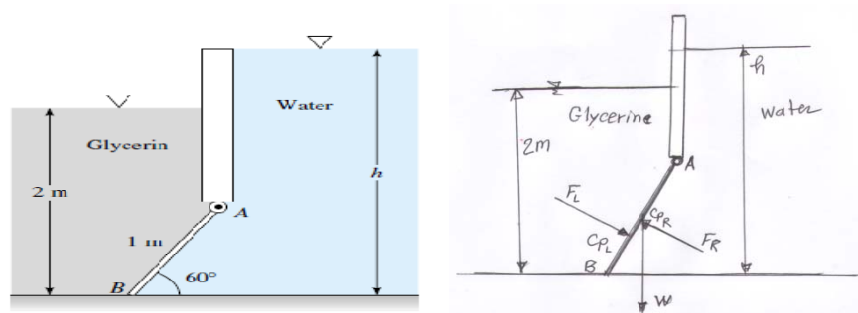
$$P_A + \rho_{\text{Benzene}} g(0.2) - \rho_{\text{Hg}} g(0.08) - \rho_{\text{kerosene}} g(0.32) + \rho_w g(0.26) = P_B$$

$$\therefore P_B = 10^5 + 881 \times 9.81 \times 0.2 - 13600 \times 9.81 \times 0.08 - 0.804 \times 9810 \times 0.32 + 9810 \times 0.26$$

$$\therefore P_B = 91082 \text{ Pa} = 0.91082 \text{ bar}$$

$$\therefore P_B = 13.20688 \text{ psi}$$

b)



The left hand force acting by Glycerin
 $F_L = \rho g h_{ce} A = 1264 \times 9.81 \times (2 - 0.5 \sin 60) \times 1 \times 1.2$
 $= 23.3165 \text{ KN}$
 $Y_{ccl} = 1.8094 \text{ m}$
 $Y_{cpl} = Y_{ccl} + \frac{(1.2)(1)}{12 \times 1.8049 \times 1.2} = 1.85557 \text{ m}$
 The Distance between c_{pl} and A

$$= 0,54617 \text{ m}$$

The Right-hand force exerts by water

$$F_R = 9810 \times (h - 0,55 \sin 60) \times 1,2 \text{ N}$$

$$Y_{CPR} = Y_{CGR} + \frac{1,2 \times 1^3}{12 \times Y_{CGR} \times 1,2} = (1,1547h - 0,5)$$

$$+ \frac{1,2 \times 1^3}{12 \times (1,1547h - 0,5) \times 1,2}$$

The Distance Between C_{PR} and A

$$= 0,5 + \frac{1}{12 \times (1,1547h - 0,5)}$$

Taking The moment about A

$$23,3165 \times 10^3 \times 0,54617 + 180 \times 9,81 \times 0,5 \cos 60$$

$$= 9810 \times (h - 0,5 \sin 60) \times 1,2 \times \left[0,5 + \frac{1}{12(1,1547h - 0,5)} \right]$$

$$13176,2 = 5886h - 2548,7 + \frac{981(h - 0,5 \sin 60)}{1,1547h - 0,5}$$

$$15724,92 = 5886h + \frac{981(h - 0,433)}{1,1547h - 0,5}$$

$$18157,565h - 7862,46 = 6796,56h^2$$

$$- 2943h + 981h - 424,77$$

$$\therefore 6796,56h^2 - 20119,565h + 7437,69 = 0$$

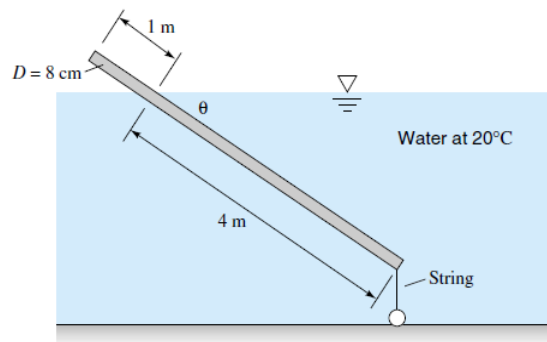
$$h^2 - 2,96257h + 1,09433 = 0$$

$$h_{1,2} = \frac{2,96257 \pm \sqrt{(2,96257)^2 - 4(1,09433)}}{2}$$

$$= 2,52724 \text{ m} \quad \text{or} \quad 0,433 \text{ m}$$

$$h = 2,52724 \text{ m}$$

2-c)



The weight of the rod is acting at the middle of the rod (C.G).

The up thrust R is acting upward at the middle of the immersed portion of the rod. Assume the tension T in the string.

From the equilibrium of forces $R = W_{rod} + T \rightarrow W_{rod} = \rho_{rod} V_{rod} g, R = \rho_{water} \times 0,8 V_{rod} g$. Assume that the rod is making an angle θ with the horizontal and taking the moment about the lower end of the rod we get

$$\rightarrow W_{rod} \times 2,5 \cos \theta = R \times 2 \cos \theta \rightarrow 2,5 \rho_{rod} V_{rod} g = 2 \rho_{water} \times 0,8 V_{rod} g \rightarrow \frac{\rho_{rod}}{\rho_{water}} = 0,64$$

The tension in the string $T = R - W_{rod} = \frac{\pi}{4} (0,08)^2 \times 4 \times 1000 \times 9,81 - \frac{\pi}{4} (0,08)^2 \times 5 \times 640 \times 9,81 = 39,448 \text{ N}$

3-a) i-

$$\vec{V} = 10x^2\mathbf{i} - 20xy\mathbf{j} + 100t\mathbf{k}$$

$$\vec{V} = u\mathbf{i} + v\mathbf{j} + w\mathbf{k} \rightarrow u = 10x^2, v = -20xy, w = 100t$$

At the point (1,2,5) and time t=0.1sec, the velocity is;

$$\vec{V} = 10\mathbf{i} - 40\mathbf{j} + 10\mathbf{k}$$

the acceleration $\vec{a} = a_x\mathbf{i} + a_y\mathbf{j} + a_z\mathbf{k}$

$$a_x = \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} \rightarrow a_x = 0 + (10x^2)(20x) + (-20xy)(0) + 100t(0) = 200x^3$$

$$a_y = \frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} \rightarrow a_y = 0 + (10x^2)(-20y) + (-20xy)(-20x) + 100t(0) = -200x^2y + 400x^2y = +200yx^2$$

$$a_z = \frac{\partial w}{\partial t} + u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z} \rightarrow a_z = 100 + (10x^2)(0) + (-20xy)(0) + 100t(0) = 100$$

At the point (1,2,5) and time t=0.1sec, the acceleration is;

$$a_x = 200, a_y = 400, a_z = 100 \rightarrow \vec{a} = 200\mathbf{i} + 400\mathbf{j} + 100\mathbf{k}$$

At time t=0

$$\vec{V} = u\mathbf{i} + v\mathbf{j} + w\mathbf{k} \rightarrow u = 10x^2, v = -20xy, w = 0$$

$$\frac{dy}{dx} = \frac{v}{u} = \frac{-20xy}{10x^2} = \frac{-2y}{x}$$

$$2ydy + xdx = 0 \rightarrow y^2 + \frac{x^2}{2} = \text{const} = 4.5$$

iii) The vorticity is given by : $\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} = -20y - 0 = -40\text{S}^{-1}$

3-b)i)

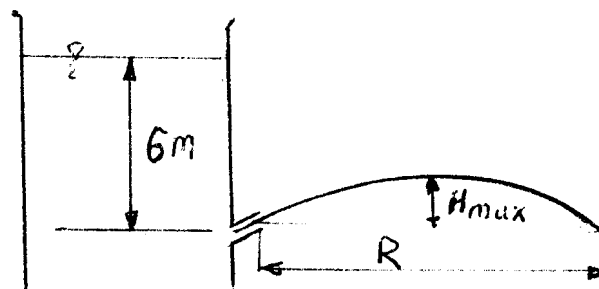


Figure 4

The maximum height H_{\max} is given from the relation;

$$H_{\max} = H \sin^2\theta = 6.0 \times 0.25 = 1.5 \text{ m};$$

The range R is given by the equation: $R = 2H \sin 2\theta \rightarrow R = 2 \times 6 \times \sin 60^\circ$

$$R = 6\sqrt{3} = 10.392 \text{ m}$$

ii) The time to empty the tank is calculated as follows:

$$-A_T \frac{dh}{dt} = C_d A_o \sqrt{2gh} \rightarrow dt = -\frac{A_T}{C_d A_o \sqrt{2g}} \frac{dh}{\sqrt{h}}$$

$$t = -\frac{A_T}{C_d A_o \sqrt{2g}} \int_6^0 \frac{dh}{\sqrt{h}} = -\frac{2A_T \sqrt{h}}{C_d A_o \sqrt{2g}} \Big|_6^0 \rightarrow t = 737.34 \text{ sec}$$

3-c

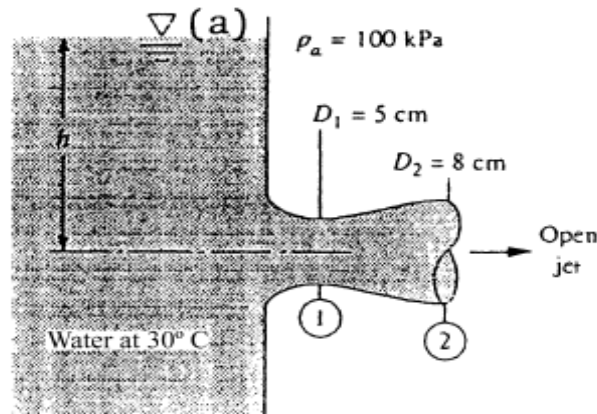


Figure 5

Applying Bernoulli equation between point a and the exit section 2

$$V_2 = \sqrt{2gh}; \text{ and from the continuity equation } V_1 = \left(\frac{D_2^2}{D_1^2}\right)V_2 = \frac{64}{25}\sqrt{2gh}$$

And applying Bernoulli equation between point 1 and 2

$$\frac{p_2}{\rho g} + \frac{V_2^2}{2g} + Z_2 = \frac{p_1}{\rho g} + \frac{V_1^2}{2g} + Z_1$$

$$\frac{101325}{9810} + h + 0 = \frac{2340}{9810} + 7.1111111h + 0$$

$$h = 1.65113 \text{ m}$$

4-a)

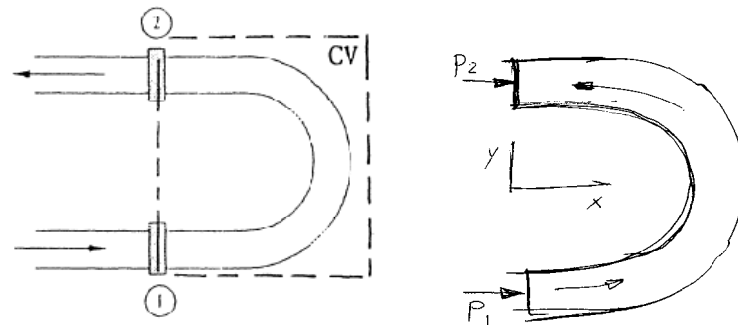


Figure 6

$$\sum F_x = \dot{m} u_{out} - \dot{m} u_{in}$$

$$u = \frac{Q}{A} = 11.7138 \text{ m/sec}$$

$$(P_1 + P_2)A + R_x = 23 \cdot [-11.7138 - 11.7138]$$

$$(165 + 134) \times 10^3 \times 1.963495 \times 10^{-3} - R_x = -538.8348$$

$$R_x = 538.8348 + 507.085 = 1045.92 \text{ N}$$

$$\sum F_y = \dot{m} v_{out} - \dot{m} v_{in}$$

$$-m_{water}g + R_y = 0 \Rightarrow R_y = 5gAL = 14.446 \text{ N}$$

$$R = \sqrt{R_x^2 + R_y^2} = 1126 \text{ N} \quad \phi = \tan^{-1} \frac{R_y}{R_x} = 0.0764^\circ$$

b)

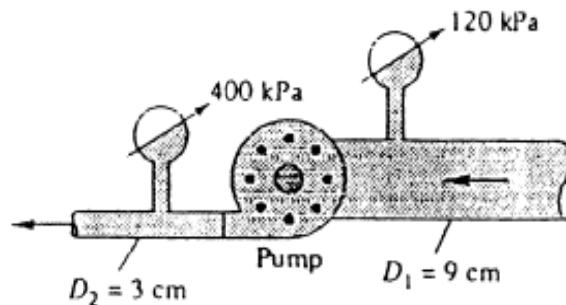


Figure 7

Applying Bernoulli equation between 1 and 2

$$\frac{p_1}{\rho g} + \frac{v_1^2}{2g} + z_1 + h_p = \frac{p_2}{\rho g} + \frac{v_2^2}{2g} + z_2$$

$$h_p = \frac{p_2 - p_1}{\rho g} + \frac{v_2^2 - v_1^2}{2g}$$

The changes in z is negligible; i.e. $z_1 = z_2$

$$v_1 = \frac{Q}{A_1} = 2.4888 \text{ m/sec},$$

$$v_2 = \frac{Q}{A_2} = 22.4 \text{ m/sec}$$

Assume the x -direction is normal to the plate and opposite to F , and the y -direction is parallel to the plate and in the direction of Q_1 .

There is no force acting on the plate in the y-direction; the only force is normal to the plate as shown in the above figure.

$$V_1 = \frac{Q}{A_1} = 2.4888 \text{ m/sec},$$

$$V_2 = \frac{Q}{A_2} = 22.4 \text{ m/sec}$$

$$h_p = 28.5423 + 25.25725 = 53.8 \text{ m}$$

$$\begin{aligned} \text{Pump power} &= 8356.4 \text{ Watt} \\ &= 11.356 \text{ HP} \end{aligned}$$

5-a)

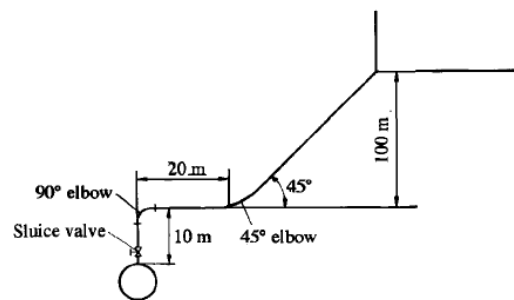


Figure 7

$$\text{The speed of flow inside the pipe is given by } v = \frac{Q}{A} = \frac{60}{\pi \frac{0.1^2}{4}} = 2.122 \text{ m/sec}$$

$$\text{The total length of the pipe is } L = 10 + 20 + 100\sqrt{2} = 171.14 \text{ m}$$

$$\text{The losses at the pipe outlet is } \frac{v^2}{2g}$$

Assume z_1 at pump outlet is 0, so z_2 is 110 m

Applying the energy equation $h_p = z_2 - z_1 + h_f + h_m$, where h_f is the friction losses given by:

$$h_f = \frac{fL}{D} \frac{v^2}{2g} \text{ and } h_m \text{ is the local losses given by: } h_m = (k_v + k_{90} + k_{45} + 1) \times \frac{v^2}{2g}$$

$$h_f = \frac{fL}{D} \frac{v^2}{2g} = 9.82 \text{ m, and } h_m = (k_v + k_{90} + k_{45} + 1) \times \frac{v^2}{2g} = 0.6334 \text{ m}$$

$$h_p = z_2 - z_1 + h_f + h_m = 110 + 9.82 + 0.6334 = 120.453 \text{ m}$$

$$\text{Pump horse power} = 19.694 \text{ kW}$$

$$\text{Brake horse power} = 24.61767 \text{ kW}$$

b) We have $m = 7$ physical parameters : deflection , δ , wire length l , speed of fluid , v , diameter of wire , d , fluid density , ρ , fluid viscosity , μ , and modulus of elasticity , E .

We have $n=3$ (three basic dimensions L, M, and T).

Dimensions of the physical parameters:

$$\begin{aligned}
\delta &: [L] \\
l &: [L] \\
v &: [L T^{-1}] \\
\rho &: [ML^{-3}] \\
\mu &: [ML^{-1}T^{-1}] \\
d &: [L] \\
E &: [ML^{-1}T^{-2}]
\end{aligned}$$

We have m-n=3 π groups $\pi_1, \pi_2, \pi_3, \pi_4$, i.e $\Phi(\pi_1, \pi_2, \pi_3, \pi_4) = 0$

Choose ρ, l, v as repeating variables ,

$$(\pi_1 = \delta \rho^{a_1} l^{b_1} v^{c_1}, \pi_2 = d \rho^{a_2} l^{b_2} v^{c_2}, \pi_3 = \mu \rho^{a_3} l^{b_3} v^{c_3}, \pi_4 = E \rho^{a_4} l^{b_4} v^{c_4})$$

$$\text{-For } \pi_1 = \delta \rho^{a_1} l^{b_1} v^{c_1} \rightarrow M^0 L^0 T^0 = [L][ML^{-3}]^{a_1} [L]^{b_1} [LT^{-1}]^{c_1}$$

$$\text{For } M \rightarrow 0 = a_1 \rightarrow a_1 = 0$$

$$\text{For } L \rightarrow 0 = 1 - 3a_1 + b_1 + c_1 = 1 + b_1 + c_1$$

$$\text{For } T \rightarrow 0 = 0 - c_1 \rightarrow c_1 = 0 \rightarrow \pi_1 = \frac{\delta}{l}$$

$$\text{-For } \pi_2 = Q \rho^{a_2} N^{b_2} D^{c_2} \rightarrow M^0 L^0 T^0 = [L^3 T^{-1}][ML^{-3}]^{a_2} [T^{-1}]^{b_2} [L]^{c_2}$$

$$\text{For } M \rightarrow 0 = 0 + a_2 \rightarrow a_2 = 0$$

$$\text{For } L \rightarrow 0 = 3 - 3a_2 + c_2 \rightarrow c_2 = -3$$

$$\text{For } T \rightarrow 0 = -1 - b_1 \rightarrow b_1 = -1 \rightarrow \pi_2 = \frac{Q}{D^3 N}$$

$$\text{-For } \pi_3 = gh \rho^{a_3} N^{b_3} D^{c_3} \rightarrow M^0 L^0 T^0 = [L^2 T^{-2}][ML^{-3}]^{a_3} [T^{-1}]^{b_3}$$

$$\text{For } M \rightarrow 0 = 0 + a_3 \rightarrow a_3 = 0$$

$$\text{For } L \rightarrow 0 = 2 - 3a_3 + c_3 \rightarrow c_3 = -2$$

$$\text{For } T \rightarrow 0 = -2 - b_1 \rightarrow b_1 = -2 \rightarrow \pi_3 = \frac{gh}{N^2 D^2} \text{ so we have three non-dimensional grouping:}$$

$$\pi_1 = \frac{P}{\rho N^3 D^5}, \pi_2 = \frac{Q}{D^3 N}, \text{ and } \pi_3 = \frac{gh}{N^2 D^2}$$